



PDHonline Course E426 (3 PDH)

Voltage Drop Calculations

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Table 2

| Derivation of Value K for Copper Using NEC Table 8 | | | |
|---|---|---|---------------------------------------|
| Wire Size (Stranded) | NEC Table 8 Circular Mils (C.M.) | NEC Table 8 DC Ohms per 1,000 ft | DC Ohms*C.M./ft |
| 12 | 6,530 | 1.98 | 12.929 |
| 10 | 10,380 | 1.24 | 12.871 |
| 8 | 16,510 | 0.778 | 12.845 |
| 6 | 26,240 | 0.491 | 12.884 |
| 4 | 41,740 | 0.308 | 12.856 |
| 2 | 66,360 | 0.194 | 12.874 |
| 1 | 83,690 | 0.154 | 12.888 |
| 1/0 | 105,600 | 0.122 | 12.883 |
| 2/0 | 133,100 | 0.0967 | 12.871 |
| 250 | 250,000 | 0.0515 | 12.875 |
| 350 | 350,000 | 0.0367 | 12.845 |
| 500 | 500,000 | 0.0258 | 12.900 |
| | | | 12.877 Average Value |

| Comparison to NEC Table 9 in Steel Conduit | | | | | |
|---|---|---|----------------------------|--|--|
| Wire Size (Stranded) | NEC Table 8 Circular Mils (C.M.) | NEC Table 9 AC Ohms per 1,000 ft | AC Ohms*C.M./ft | NEC Table 9 Effective Z at 0.85 PF per 1,000 ft | Effective Z at 0.85 PF Ohms*C.M./ft |
| 12 | 6,530 | 2.0 | 13.060 | 1.7 | 11.101 |
| 10 | 10,380 | 1.2 | 12.456 | 1.1 | 11.418 |
| 8 | 16,510 | 0.78 | 12.878 | 0.70 | 11.557 |
| 6 | 26,240 | 0.49 | 12.858 | 0.45 | 11.808 |
| 4 | 41,740 | 0.31 | 12.939 | 0.30 | 12.522 |
| 2 | 66,360 | 0.20 | 13.272 | 0.20 | 13.272 |
| 1 | 83,690 | 0.16 | 13.390 | 0.16 | 13.390 |
| 1/0 | 105,600 | 0.12 | 12.672 | 0.13 | 13.728 |
| 2/0 | 133,100 | 0.10 | 13.310 | 0.11 | 14.641 |
| 250 | 250,000 | 0.054 | 13.500 | 0.073 | 18.250 |
| 350 | 350,000 | 0.039 | 13.650 | 0.060 | 21.000 |
| 500 | 500,000 | 0.029 | 14.500 | 0.050 | 25.000 |

Table 3

| Effective Z at 0.85 PF for Selected Wire Sizes in Steel Conduit | | | | | | |
|---|-------------------|--------------------------------|-----------------------------------|------------------|------------------|---|
| Wire Size | X_L (Reactance) | Alternating-Current Resistance | Power Factor PF [cos(θ)] | Rcos(θ) | Xsin(θ) | Effective Z = Rcos(θ) + Xsin(θ) |
| 12 | 0.068 | 2.0 | 0.85 | 1.700 | 0.036 | 1.7 |
| 10 | 0.063 | 1.2 | 0.85 | 1.020 | 0.033 | 1.1 |
| 4 | 0.060 | 0.31 | 0.85 | 0.264 | 0.032 | 0.30 |
| 2 | 0.057 | 0.20 | 0.85 | 0.170 | 0.030 | 0.20 |
| 1/0 | 0.055 | 0.12 | 0.85 | 0.102 | 0.029 | 0.13 |
| 250 | 0.052 | 0.054 | 0.85 | 0.046 | 0.027 | 0.073 |
| 500 | 0.048 | 0.029 | 0.85 | 0.025 | 0.025 | 0.050 |

Table 4

| Effective Z at Selected PF for Selected Wire Sizes in Steel Conduit | | | | | | |
|---|-------------------|--------------------------------|-----------------------------------|------------------|------------------|---|
| Wire Size | X_L (Reactance) | Alternating-Current Resistance | Power Factor PF [cos(θ)] | Rcos(θ) | Xsin(θ) | Effective Z = Rcos(θ) + Xsin(θ) |
| 12 | 0.068 | 2.000 | 0.80 | 1.600 | 0.041 | 1.641 |
| 12 | 0.068 | 2.000 | 0.85 | 1.700 | 0.036 | 1.736 |
| 12 | 0.068 | 2.000 | 0.90 | 1.800 | 0.030 | 1.830 |
| 12 | 0.068 | 2.000 | 1.00 | 2.000 | 0.000 | 2.000 |
| 10 | 0.063 | 1.200 | 0.80 | 0.960 | 0.038 | 0.998 |
| 10 | 0.063 | 1.200 | 0.85 | 1.020 | 0.033 | 1.053 |
| 10 | 0.063 | 1.200 | 0.90 | 1.080 | 0.027 | 1.107 |
| 10 | 0.063 | 1.200 | 1.00 | 1.200 | 0.000 | 1.200 |
| 4 | 0.060 | 0.310 | 0.80 | 0.248 | 0.036 | 0.284 |
| 4 | 0.060 | 0.310 | 0.85 | 0.264 | 0.032 | 0.295 |
| 4 | 0.060 | 0.310 | 0.90 | 0.279 | 0.026 | 0.305 |
| 4 | 0.060 | 0.310 | 1.00 | 0.310 | 0.000 | 0.310 |
| 2 | 0.057 | 0.200 | 0.80 | 0.160 | 0.034 | 0.194 |
| 2 | 0.057 | 0.200 | 0.85 | 0.170 | 0.030 | 0.200 |
| 2 | 0.057 | 0.200 | 0.90 | 0.180 | 0.025 | 0.205 |
| 2 | 0.057 | 0.200 | 1.00 | 0.200 | 0.000 | 0.200 |
| 1/0 | 0.055 | 0.120 | 0.80 | 0.096 | 0.033 | 0.129 |
| 1/0 | 0.055 | 0.120 | 0.85 | 0.102 | 0.029 | 0.131 |
| 1/0 | 0.055 | 0.120 | 0.90 | 0.108 | 0.024 | 0.132 |
| 1/0 | 0.055 | 0.120 | 1.00 | 0.120 | 0.000 | 0.120 |
| 250 | 0.052 | 0.054 | 0.80 | 0.043 | 0.031 | 0.074 |
| 250 | 0.052 | 0.054 | 0.85 | 0.046 | 0.027 | 0.073 |
| 250 | 0.052 | 0.054 | 0.90 | 0.049 | 0.023 | 0.071 |
| 250 | 0.052 | 0.054 | 1.00 | 0.054 | 0.000 | 0.054 |
| 500 | 0.048 | 0.029 | 0.80 | 0.023 | 0.029 | 0.052 |
| 500 | 0.048 | 0.029 | 0.85 | 0.025 | 0.025 | 0.050 |
| 500 | 0.048 | 0.029 | 0.90 | 0.026 | 0.021 | 0.047 |
| 500 | 0.048 | 0.029 | 1.00 | 0.029 | 0.000 | 0.029 |

Table 5

| Vdrop Error for 10 Hp at 480V/3Φ, 0.85 PF | | | | | | | | | | | |
|---|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|--------------------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 12 | 6,530 | 1.98 | 0.068 | 2.000 | 0.85 | 1.700 | 0.036 | 1.700 | 1.736 | 14.0 | 200.0 |
| Equation 11: Error = {Vs - √[Vs ² - (IXcosΦ-IRsinΦ) ²]} | | | | | | | | | Result: | 0.0140 V Error line-to-neutral | |
| Equation 15: Error = √3*{Vs - √[Vs ² - (IXcosΦ-IRsinΦ) ²]} | | | | | | | | | Result: | 0.0243 V Error line-to-line | |

| Vdrop Error for 15 KW at 480V/3Φ, 1.0 PF | | | | | | | | | | | |
|---|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|--------------------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 10 | 10,380 | 1.24 | 0.063 | 1.200 | 1.00 | 1.200 | 0.000 | 1.100 | 1.200 | 18.0 | 200.0 |
| Equation 11: Error = {Vs - √[Vs ² - (IXcosΦ-IRsinΦ) ²]} | | | | | | | | | Result: | 0.0001 V Error line-to-neutral | |
| Equation 15: Error = √3*{Vs - √[Vs ² - (IXcosΦ-IRsinΦ) ²]} | | | | | | | | | Result: | 0.0002 V Error line-to-line | |

| Vdrop Error for 250 Hp at 480V/3Φ, 0.9 PF | | | | | | | | | | | |
|---|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|-------------------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 500 | 500,000 | .0258 | 0.048 | 0.029 | 0.90 | 0.026 | 0.021 | 0.050 | 0.047 | 302.0 | 200.0 |
| Equation 11: Error = {Vs - √[Vs ² - (IXcosΦ-IRsinΦ) ²]} | | | | | | | | | Result: | 0.006 V Error line-to-neutral | |
| Equation 15: Error = √3*{Vs - √[Vs ² - (IXcosΦ-IRsinΦ) ²]} | | | | | | | | | Result: | 0.011 V Error line-to-line | |

Table 7

| Comparing the Results of Different Line-to-Line Vdrop Formulas for 10 Hp at 480V/3Φ, 0.85 PF | | | | | | | | | | | |
|--|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 12 | 6,530 | 1.98 | 0.068 | 2.000 | 0.85 | 1.700 | 0.036 | 1.700 | 1.736 | 14.0 | 200.0 |
| Equation 4: $V_{drop} = \sqrt{3} * I * K * R * L / A$ See Note below. $K = 12.9$ Result: 9.581 V Approx. 1.995% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using DC Ohms Only Result: 9.602 V Approx. 2% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using AC Ohms Only Result: 9.699 V Approx. 2.02% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using Effective Z at 0.85 PF Result: 8.245 V Approx. 1.717% | | | | | | | | | | | |
| Equation 9: $V_{drop} = \sqrt{3} * (IR\cos\theta + Ix\sin\theta) * L$ Calculated Effective Z Result: 8.418 V Estimated 1.753% | | | | | | | | | | | |
| Equation 16: $V_{drop} = \sqrt{3} * \{V_s + IRL\cos\theta + IXL\sin\theta - \sqrt{[V_s^2 - (IXL\cos\theta - IRL\sin\theta)^2]}\}$ $V_s = 277V$ line-to-neutral Result: 8.443 V Actual 1.758% | | | | | | | | | | | |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.

Table 8

| Comparing the Results of Different Line-to-Line Vdrop Formulas for 15 KW at 480V/3Φ, 1.0 PF | | | | | | | | | | | |
|--|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 10 | 10,380 | 1.24 | 0.063 | 1.200 | 1.00 | 1.200 | 0.000 | 1.100 | 1.200 | 18.0 | 200.0 |
| Equation 4: $V_{drop} = \sqrt{3} * I * K * R * L / A$ See Note below. K = 12.9 Result: 7.749 V Approx. 1.614% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using DC Ohms Only Result: 7.732 V Approx. 1.61% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using AC Ohms Only Result: 7.482 V Approx. 1.558% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using Effective Z at 0.85 PF Result: 6.859 V Approx. 1.428% | | | | | | | | | | | |
| Equation 9: $V_{drop} = \sqrt{3} * (IRcos\theta + Ixsin\theta) * L$ Calculated Effective Z Result: 7.482 V Estimated 1.558% | | | | | | | | | | | |
| Equation 16: $V_{drop} = \sqrt{3} * \{Vs + IRLcos\theta + IXLsin\theta - \sqrt{[Vs^2 - (IXLcos\theta - IRLsin\theta)^2]}\}$ Vs = 277V line-to-neutral Result: 7.4826 V Actual 1.558% | | | | | | | | | | | |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.

Table 9

| Comparing the Results of Different Line-to-Line Vdrop Formulas for 250 Hp at 480V/3Φ, 0.9 PF | | | | | | | | | | | |
|---|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 500 | 500,000 | .0258 | 0.048 | 0.029 | 0.90 | 0.026 | 0.021 | 0.050 | 0.047 | 302.0 | 200.0 |
| Equation 4: $V_{drop} = \sqrt{3} * I * K * R * L / A$ See Note below. K = 12.9 Result: 2.699 V Approx. 0.562% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using DC Ohms Only Result: 2.699 V Approx. 0.562% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using AC Ohms Only Result: 3.034 V Approx. 0.632% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using Effective Z at 0.85 PF Result: 5.231 V Approx. 1.089% | | | | | | | | | | | |
| Equation 9: $V_{drop} = \sqrt{3} * (IRcos\theta + Ixsin\theta) * L$ Calculated Effective Z Result: 4.919 V Estimated 1.024% | | | | | | | | | | | |
| Equation 16: $V_{drop} = \sqrt{3} * \{Vs + IRLcos\theta + IXLsin\theta - \sqrt{[Vs^2 - (IXLcos\theta - IRLsin\theta)^2]}\}$ Vs = 277V line-to-neutral Result: 4.930 V Actual 1.027% | | | | | | | | | | | |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.

Table 10

| Line-to-Line Vdrop for 10 A, 0.9 PF with 100' of 10 AWG Conductors | | | | | | | | | | 120 V/1Φ | |
|--|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 10 | 10,380 | 1.24 | 0.063 | 1.200 | 0.90 | 1.080 | 0.027 | 1.100 | 1.107 | 10.0 | 100.0 |
| Equation 4: $V_{drop} = 2 * I * K * R * L / A$ | | | | | | K = 12.9 | | Result: | | 2.486 V Approx. | 2.071% |
| Equation 3: $V_{drop} = 2 * I * R * L$ | | | | | | Using DC Ohms Only | | Result: | | 2.480 V Approx. | 2.066% |
| Equation 3: $V_{drop} = 2 * I * R * L$ | | | | | | Using AC Ohms Only | | Result: | | 2.400 V Approx. | 2% |
| Equation 3: $V_{drop} = 2 * I * R * L$ | | | | | | Using Effective Z at 0.85 PF | | Result: | | 2.200 V Approx. | 1.833% |
| Equation 9: $V_{drop} = 2 * (IRcosθ + Ixsinθ) * L$ | | | | | | Calculated Effective Z | | Result: | | 2.215 V Estimated | 1.845% |
| Equation 16: $V_{drop} = 2 * \{V_s + IRLcosθ + IXLsinθ - \sqrt{V_s^2 - (IXLcosΦ - IRLsinΦ)^2}\}$ | | | | | | V _s = 277V line-to-neutral | | Result: | | 2.216 V Actual | 1.846% |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.

Table 11

| Line-to-Line Vdrop for 10 A, 0.9 PF at One-Way Cable Length in Feet = Applied Voltage | | | | | | | | | | 120 V/1Φ | |
|--|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 12 | 6,530 | 1.98 | 0.068 | 2.000 | 0.90 | 1.800 | 0.030 | 1.700 | 1.830 | 10.0 | 120.0 |
| Equation 4: $V_{drop} = 2 * I * K * R * L / A$ | | | | | | K = 12.9 | | Result: | | 4.741 V Approx. | 3.95% |
| Equation 3: $V_{drop} = 2 * I * R * L$ | | | | | | Using DC Ohms Only | | Result: | | 4.752 V Approx. | 3.96% |
| Equation 3: $V_{drop} = 2 * I * R * L$ | | | | | | Using AC Ohms Only | | Result: | | 4.800 V Approx. | 4% |
| Equation 3: $V_{drop} = 2 * I * R * L$ | | | | | | Using Effective Z at 0.85 PF | | Result: | | 4.080 V Approx. | 3.4% |
| Equation 9: $V_{drop} = 2 * (IRcosθ + Ixsinθ) * L$ | | | | | | Calculated Effective Z | | Result: | | 4.391 V Estimated | 3.659% |
| Equation 16: $V_{drop} = 2 * \{V_s + IRLcosθ + IXLsinθ - \sqrt{[V_s^2 - (IXLcosΦ - IRLsinΦ)^2]}\}$ | | | | | | V _s = 120V line-to-neutral | | Result: | | 4.399 V Actual | 3.665% |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.

Table 12

| Line-to-Line Vdrop for 10 A, 0.9 PF at One-Way Cable Length in Feet = Applied Voltage | | | | | | | | | | 208 V/3Φ | |
|--|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 12 | 6,530 | 1.98 | 0.068 | 2.000 | 0.90 | 1.800 | 0.030 | 1.700 | 1.830 | 10.0 | 208.0 |
| Equation 4: $V_{drop} = \sqrt{3} * I * K * R * L / A$ K = 12.9 Result: 7.117 V Approx. 3.421% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using DC Ohms Only Result: 7.133 V Approx. 3.429% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using AC Ohms Only Result: 7.205 V Approx. 3.464% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using Effective Z at 0.85 PF Result: 6.125 V Approx. 2.944% | | | | | | | | | | | |
| Equation 9: $V_{drop} = \sqrt{3} * (IRcos\theta + Ixsin\theta) * L$ Calculated Effective Z Result: 6.592 V Approx. 3.169% | | | | | | | | | | | |
| Equation 16: $V_{drop} = \sqrt{3} * \{Vs + IRLcos\theta + IXLsin\theta - \sqrt{[Vs^2 - (IXLcos\Phi - IRLsin\Phi)^2]}\}$ Vs = 120V line-to-neutral Result: 6.612 V (Actual) 3.178% | | | | | | | | | | | |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.

Table 13

| Line-to-Line Vdrop for 10 A, 0.9 PF at One-Way Cable Length in Feet = Applied Voltage | | | | | | | | | | 277 V/1Φ | |
|---|---|--------------------|--|-----------------------------|--------------------------------|---------------------------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 12 | 6,530 | 1.98 | 0.068 | 2.000 | 0.90 | 1.800 | 0.030 | 1.700 | 1.830 | 10.0 | 277.0 |
| Equation 4: | $V_{drop} = 2 * I * K * R * L / A$ | | | | | K = 12.9 | | Result: | 10.944 V Approx. | 3.95% | |
| Equation 3: | $V_{drop} = 2 * I * R * L$ | | | | | Using DC Ohms Only | | Result: | 10.969 V Approx. | 3.96% | |
| Equation 3: | $V_{drop} = 2 * I * R * L$ | | | | | Using AC Ohms Only | | Result: | 11.080 V Approx. | 4% | |
| Equation 3: | $V_{drop} = 2 * I * R * L$ | | | | | Using Effective Z at 0.85 PF | | Result: | 9.418 V Approx. | 3.4% | |
| Equation 9: | $V_{drop} = 2 * (IRcosθ + Ixsinθ) * L$ | | | | | Calculated Effective Z | | Result: | 10.136 V Estimated | 3.659% | |
| Equation 16: | $V_{drop} = 2 * \{V_s + IRLcosθ + IXLsinθ - \sqrt{V_s^2 - (IXLcosΦ - IRLsinΦ)^2}\}$ | | | | | V _s = 277V line-to-neutral | | Result: | 10.154 V Actual | 3.665% | |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.

Table 14

| Line-to-Line Vdrop for 10 A, 0.9 PF at One-Way Cable Length in Feet = Applied Voltage | | | | | | | | | | 480 V/3Φ | |
|---|----------------------|--------------------|--|-----------------------------|--------------------------------|---------------------|---------------------|----------------------------------|--|----------------------|-----------------------------|
| Wire Size | Table 8 Cir. Mils | Table 8 DC Ohms | Table 9 X _L (React) Ohms/k-ft | Table 9 AC Ohms/k- ft | Power Factor PF [cos(θ)] | Rcos(θ) per k-ft | Xsin(θ) per k-ft | NEC Effective Z at 0.85 PF | Effective Z = Rcos(θ) + Xsin(θ) Ohms/k-ft | Full-Load Current | One-Way Wire Length (ft) |
| 12 | 6,530 | 1.98 | 0.068 | 2.000 | 0.90 | 1.800 | 0.030 | 1.700 | 1.830 | 10.0 | 480.0 |
| Equation 4: $V_{drop} = \sqrt{3} * I * K * R * L / A$ K = 12.9 Result: 16.424 V Approx. 3.421% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using DC Ohms Only Result: 16.461 V Approx. 3.429% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using AC Ohms Only Result: 16.628 V Approx. 3.464% | | | | | | | | | | | |
| Equation 3: $V_{drop} = \sqrt{3} * I * R * L$ Using Effective Z at 0.85 PF Result: 14.134 V Approx. 2.944% | | | | | | | | | | | |
| Equation 9: $V_{drop} = \sqrt{3} * (IRcos\theta + Ixsin\theta) * L$ Calculated Effective Z Result: 15.211 V Approx. 3.169% | | | | | | | | | | | |
| Equation 16: $V_{drop} = \sqrt{3} * \{Vs + IRLcos\theta + IXLsin\theta - \sqrt{[Vs^2 - (IXLcos\Phi - IRLsin\Phi)^2]}\}$ Vs = 277V line-to-neutral Result: 15.259 V (Actual) 3.178% | | | | | | | | | | | |

Note: Equation 4 above is the only equation in which the one-way wire length is not divided by 1,000, since the units of K are (Ohms*C.M.) / ft.